



Answer **four** questions. You are advised **not** to answer more than four questions: if you do, only your best four will be counted.

- 1 (i) Using the  $\varepsilon - \delta$  relation

$$\varepsilon_{ijk}\varepsilon_{lmk} = \delta_{il}\delta_{jm} - \delta_{im}\delta_{jl}$$

prove that

$$\mathbf{v} \times (\nabla \times \mathbf{v}) = \frac{1}{2} \nabla (\|\mathbf{v}\|^2) - (\mathbf{v} \cdot \nabla) \mathbf{v}. \quad (*)$$

(9 marks)

- (ii) You are given that, in cylindrical coordinates  $r, \phi, z$ , the gradient of a scalar field  $f$ , and the divergence and curl of a vector field  $\mathbf{v} = (v_r, v_\phi, v_z)$  are given by

$$\nabla f = \frac{\partial f}{\partial r} \mathbf{e}_r + \frac{1}{r} \frac{\partial f}{\partial \phi} \mathbf{e}_\phi + \frac{\partial f}{\partial z} \mathbf{e}_z,$$

$$\nabla \cdot \mathbf{v} = \frac{1}{r} \frac{\partial(rv_r)}{\partial r} + \frac{1}{r} \frac{\partial v_\phi}{\partial \phi} + \frac{\partial v_z}{\partial z}$$

$$\nabla \times \mathbf{v} = \left( \frac{1}{r} \frac{\partial v_z}{\partial \phi} - \frac{\partial v_\phi}{\partial z} \right) \mathbf{e}_r + \left( \frac{\partial v_r}{\partial z} - \frac{\partial v_z}{\partial r} \right) \mathbf{e}_\phi + \frac{1}{r} \left( \frac{\partial(rv_\phi)}{\partial r} - \frac{\partial v_r}{\partial \phi} \right) \mathbf{e}_z$$

where  $\mathbf{e}_r, \mathbf{e}_\phi$  and  $\mathbf{e}_z$  are the unit vector of the cylindrical coordinate system.

- (a) Show that vector field  $\mathbf{v}$  with the components given by

$$v_r = \frac{1}{r} \frac{\partial \psi}{\partial z}, \quad v_\phi = 0, \quad v_z = -\frac{1}{r} \frac{\partial \psi}{\partial r}. \quad (\dagger)$$

is divergence-free, i.e.  $\nabla \cdot \mathbf{v} = 0$ . (2 marks)

- (b) You are again given that vector field  $\mathbf{v}$  is defined by  $(\dagger)$ . In addition, you are given that function  $\psi$  is independent of  $\phi$ . Using  $(*)$  express  $(\mathbf{v} \cdot \nabla) \mathbf{v}$  in terms of the function  $\psi$ . (14 marks)

- 2 (i) Give the definition in words of the material derivative. Derive the expression for the material derivative of a function  $f(\mathbf{x}, t)$  in the Eulerian description,

$$\frac{Df}{Dt} = \frac{\partial f}{\partial t} + \mathbf{v} \cdot \nabla f,$$

where  $\mathbf{v}$  is the velocity.

*(7 marks)*

- (ii) The motion of the continuum is described in Lagrangian variables by

$$x_1 = \xi_1 - \alpha \xi_2 \cosh \omega t, \quad x_2 = \xi_2 + \alpha \xi_1 \sinh \omega t, \quad x_3 = \xi_3,$$

where  $\alpha$  and  $\omega$  are positive constants.

- (a) Calculate the Jacobian  $J$  of the transformation from  $\boldsymbol{\xi}$  to  $\mathbf{x}$ .

*(6 marks)*

- (b) Obtain the expression for the velocity field  $\mathbf{v}$  in the Lagrangian and Eulerian variables.

*(12 marks)*

- 3 (i) Write down the expression for the surface traction,  $\mathbf{t}$ , in terms of the stress tensor,  $\mathbf{T}$ , and the unit normal to the surface,  $\mathbf{n}$ . Express it both in vector and coordinate form. (3 marks)

- (ii) Show that

$$\int_S \mathbf{t} dS = \int_V \nabla \cdot \mathbf{T} dV. \quad (*)$$

where  $S$  is the surface of the volume  $V$ . (7 marks)

- (iii) Using the momentum equation written in the integral form,

$$\frac{d}{dt} \int_V \rho \mathbf{v} dV = \int_S \mathbf{t} dS + \int_V \rho \mathbf{b} dV,$$

and equation (\*), derive the momentum equation written in the differential form in Eulerian variables,

$$\rho \frac{D\mathbf{v}}{Dt} = \nabla \cdot \mathbf{T} + \rho \mathbf{b},$$

where  $\rho$  is the density,  $\mathbf{v}$  the velocity, and  $\mathbf{b}$  the body force. (You can use without derivation the formula for differentiation of an integral over a moving volume,  $\frac{d}{dt} \int_V \rho f dV = \int_V \rho \frac{Df}{Dt} dV$ , where  $f$  is an arbitrary function.) (5 marks)

- (iv) You are given that a continuum occupies the half-space  $z > 0$  in Cartesian coordinates  $x, y, z$ . There is a constant body force in the negative  $z$ -direction,  $\mathbf{b} = (0, 0, -g)$ . You are also given that the stress tensor has the form  $\mathbf{T} = -p\mathbf{I}$ , where  $\mathbf{I}$  is the unit tensor and  $p$  the pressure. The pressure  $p$  is proportional to the continuum density  $\rho$ ,  $p = \alpha\rho$ , and  $p = p_0 = \text{const}$  at  $z = 0$ . Determine the dependence of  $p$  on  $z$ . (10 marks)

- 4 (i) Give the definition of ideal incompressible fluid. Use the mass conservation equation written in Lagrangian variables to show that the density of an incompressible fluid satisfies the equation

$$\frac{D\rho}{Dt} = 0.$$

Use the mass conservation equation written in Eulerian variables to show that the velocity of this fluid satisfies the equation

$$\nabla \cdot \mathbf{v} = 0.$$

When this fluid is called homogeneous? **(10 marks)**

- (ii) The fluid motion is called planar when, in Cartesian coordinates  $x, y, z$ , the  $z$ -component of the fluid velocity is zero while the  $x$  and  $y$ -component are independent of  $z$ . Show that the velocity of planar motion of an incompressible fluid can be expressed in terms of the flux function  $\psi$  as

$$v_x = \frac{\partial \psi}{\partial y}, \quad v_y = -\frac{\partial \psi}{\partial x}.$$

**(7 marks)**

- (iii) Give the definition of a streamline. Show that streamlines of a planar motion of an incompressible fluid are defined by the equation

$$\psi(x, y) = \text{const.}$$

(You can use without derivation that the general equation of a streamline is  $\frac{dx}{v_x} = \frac{dy}{v_y} = \frac{dz}{v_z}$ .) **(3 marks)**

- (iv) The fluid motion is called potential when  $\mathbf{v} = \nabla\varphi$ , where  $\varphi$  is called the potential. Show that the flux function of a potential planar motion of an ideal incompressible fluid satisfies the Laplace equation

$$\nabla^2\psi = 0.$$

**(5 marks)**

- 5 (i) In the linear elasticity the equilibrium of an isotropic material is described by the equation

$$(\lambda + \mu)\nabla(\nabla \cdot \mathbf{u}) + \mu\nabla^2\mathbf{u} + \rho\mathbf{b} = 0. \quad (*)$$

You are given that, in cylindrical coordinates  $r, \phi, z$ , the displacement vector  $\mathbf{u}$  has only the  $\phi$ -component and it is independent of  $\phi$ ,  $\mathbf{u} = (0, u(r, z), 0)$ . In addition, there is no body force,  $\mathbf{b} = 0$ . Show that, in this case, equation (\*) reduces to

$$\frac{\partial}{\partial r} \frac{1}{r} \frac{\partial(ru)}{\partial r} + \frac{\partial^2 u}{\partial z^2} = 0. \quad (\dagger)$$

You can use without proof the formulae

$$\nabla \cdot \mathbf{u} = \frac{1}{r} \frac{\partial(ru_r)}{\partial r} + \frac{1}{r} \frac{\partial u_\phi}{\partial \phi} + \frac{\partial u_z}{\partial z},$$

$$\nabla^2 \mathbf{u} = \nabla(\nabla \cdot \mathbf{u}) - \nabla \times \nabla \times \mathbf{u},$$

$$\nabla \times \mathbf{u} = \left( \frac{1}{r} \frac{\partial u_z}{\partial \phi} - \frac{\partial u_\phi}{\partial z} \right) \mathbf{e}_r + \left( \frac{\partial u_r}{\partial z} - \frac{\partial u_z}{\partial r} \right) \mathbf{e}_\phi + \frac{1}{r} \left( \frac{\partial(ru_\phi)}{\partial r} - \frac{\partial u_r}{\partial \phi} \right) \mathbf{e}_z.$$

(6 marks)

- (ii) There is an elastic rod of radius  $R$  and length  $L$ . The rod axis coincides with the  $z$ -axis of cylindrical coordinates. Its ends are fixed at the planes  $z = 0$  and  $z = L$ . Initially there are no stresses in the rod. Then the upper plane is rotated by a small angle  $\alpha$ , so the displacement at  $z = L$  is  $\mathbf{u} = (0, \alpha r, 0)$ . The lower plane does not move, so the displacement is zero at  $z = 0$ . You can assume that the displacement in the rod has the form  $\mathbf{u} = (0, u(r, z), 0)$ , so it is described by equation ( $\dagger$ ). Looking for the solution to this equation in the form  $u = rf(z)$ , determine the function  $f(z)$ . (5 marks)

- (iii) Use the expression of the stress tensor in terms of the displacement,

$$\mathbf{T} = \lambda \mathbf{I} \nabla \cdot \mathbf{u} + \mu [\nabla \mathbf{u} + (\nabla \mathbf{u})^T],$$

where  $\mathbf{I}$  is the unit tensor to calculate the stress tensor inside the rod. You can use without proof that, for  $\mathbf{u} = (0, u(r, z), 0)$ ,

$$\nabla \mathbf{u} = \frac{\partial u}{\partial r} \mathbf{e}_r \mathbf{e}_\phi - \frac{u}{r} \mathbf{e}_\phi \mathbf{e}_r + \frac{\partial u}{\partial z} \mathbf{e}_z \mathbf{e}_\phi.$$

(5 marks)

- (iv) Use the obtained expression for  $\mathbf{T}$  to calculate the surface traction at the upper edge of the rod,  $z = L$ . Then determine the moment of the force applied to the upper plane that is needed to rotate it by the angle  $\alpha$ .

(9 marks)

End of Question Paper